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# MD simulations of polymeric C<sub>60</sub> fullerene layers/chain under tension

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The molecular dynamics (MD) method based on the Tersoff potential was used to simulate the tension and fracture of three polymeric  $7 \times 7C_{60}$  fullerene layers, with no defect, one single-edge defect or one central defect, as well as one polymeric  $7C_{60}$  fullerene chain. The effects of different type defect and tensile velocity on the fracture behavior and tensile mechanical properties of the C<sub>60</sub> layers/chain were discussed and analyzed. It is shown that, (1) the C<sub>60</sub> layers, with different type defect and different tensile velocity, have different cracking positions and fracture modes; (2) the fracture strength  $\sigma_c$  and deformation capability for the presented C<sub>60</sub> layers/chain have the orders of “no-defect C<sub>60</sub> layer > single-edge defect C<sub>60</sub> layer > central defect C<sub>60</sub> layer >  $7C_{60}$  chain” and “no-defect C<sub>60</sub> layer > single-edge defect C<sub>60</sub> layer >  $7C_{60}$  chain > central defect C<sub>60</sub> layer”, respectively; (3) the C<sub>60</sub> layers/chain with high tensile-velocity have higher fracture strength  $\sigma_c$ , higher elastic module  $E$  but lower deformation capability than those with low velocity; (4) for the same tensile velocity the C<sub>60</sub> layers have higher elastic module  $E$  than the C<sub>60</sub> chain, and the no-defect C<sub>60</sub> layer has the higher  $E$  than the two other C<sub>60</sub> layers; (5) the C<sub>60</sub> layers/chain have lower  $E$  but much higher tensile strength  $\sigma_c$  than steel.

**Keywords:** C<sub>60</sub> layers/chain; Tensile properties; MD; Tensile velocity

## 1. Introduction

Carbon fullerene is a new form of carbon different from graphite and diamond. Due to its cage-like molecular configure, quantum size effect and geometric size effect, carbon fullerene shows unusual chemical, catalytic and photoelectric characters, and has extensive potential application in the fields of chemical industry, photoelectric materials and so on [1,2]. Since C<sub>60</sub> fullerene, the best known and most stable fullerene, was first found by Kroto *et al.* [3], people have made much effort in preparing fullerene and investigating its micro-structure [2,4]. Interestingly, two kinds of C<sub>60</sub> fullerene polymers, namely two-dimensional C<sub>60</sub> layer [5] and one-dimensional C<sub>60</sub> chain [6], were recently found at the high-pressure/high-temperature conditions. In the C<sub>60</sub> polymers, the adjacent C<sub>60</sub> fullerenes are bridged through a pair of parallel C–C bonds.

It is well known that nano-materials often have some peculiar properties. In order to fully utilize the nano-materials, firstly, people must thoroughly investigate their various physical and chemical characters. Now some studies on the polymeric C<sub>60</sub> layer or C<sub>60</sub> chain have been

carried out. For example, the molecular or electronic structures of the C<sub>60</sub> layer and C<sub>60</sub> chain have been characterized through the spectroscopic techniques including X-ray, IR, Raman and so on [6,7–9]. However, the mechanical properties of the polymeric C<sub>60</sub> layer or C<sub>60</sub> chain have never been reported.

Considering the above reason, in the present paper the Tersoff potential based molecular dynamics (MD) method is used to simulate the tension of three square C<sub>60</sub> single-layers and one  $7C_{60}$  chain. At last the effects of different type defect and tensile velocity on their tensile properties are discussed further. Some conclusions in the present paper are very helpful for people to cognize the mechanical characters of the one-dimensional and two-dimensional C<sub>60</sub> polymers.

## 2. The models and method

Figure 1 presents the investigated objects, three square  $7 \times 7C_{60}$  single-layers and one  $7C_{60}$  chain. Both the side-lengths  $L$  of the polymeric C<sub>60</sub> layers and the length  $L$  of the  $7C_{60}$  chain are about 6.84 nm. The C<sub>60</sub> layer in figure 1(b)

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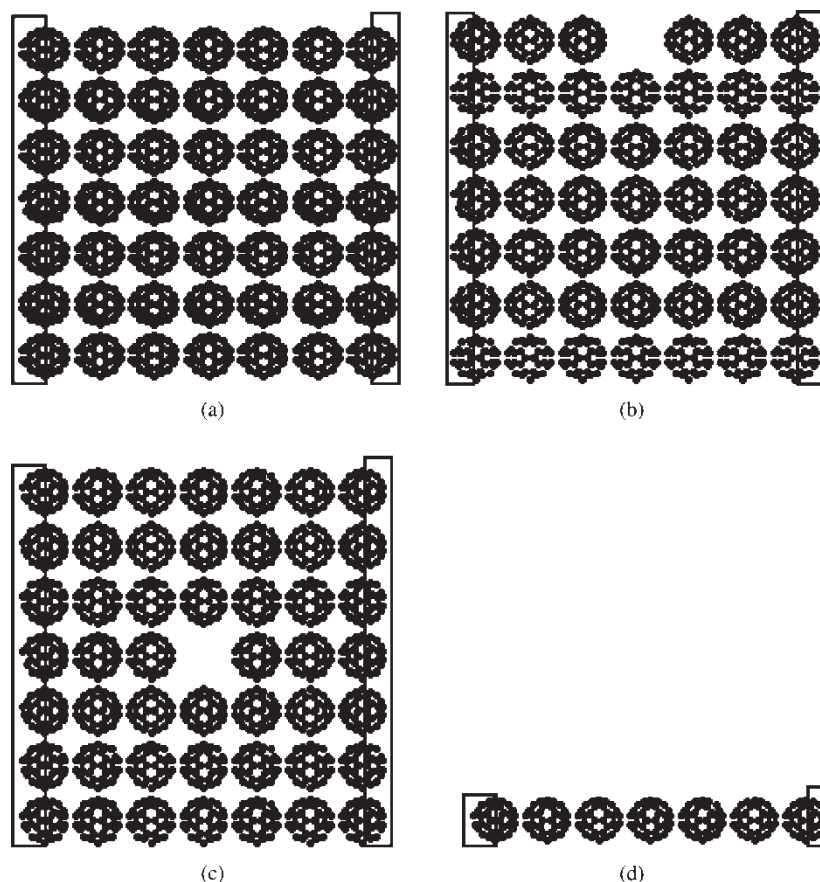


Figure 1. Polymeric C<sub>60</sub> fullerene layers/chain. (a) no-defect C<sub>60</sub> layer; (b) single-edge defect C<sub>60</sub> layer; (c) central defect C<sub>60</sub> layer; and (d) 7C<sub>60</sub> chain.

has one single-edge defect and the one in figure 1(c) one central defect, considering the fact that the defects have been found in some polymeric C<sub>60</sub> layer. Any two adjacent C<sub>60</sub> fullerenes in these C<sub>60</sub> polymers are bridged by two parallel C–C bonds and have the distance about 0.93 nm [6]. All the C<sub>60</sub> fullerenes in the C<sub>60</sub> layers/chain have the diameter of  $D \approx 0.73$  nm.

Both the molecular modeling and geometry optimization of the C<sub>60</sub> layers/chain in figure 1 are performed in the famous quantum-chemical software of HyperChem 7 [10]. In the geometry optimization, the MM+ force field and the Fletcher's conjugate gradient method [11] are adopted, and the energy convergence limit takes 0.01 Kcal/mol.

In the present paper the classical MD method is used to simulate the tension of the C<sub>60</sub> layers/chain. During the simulations the carbon atoms in the left frames of figure 1 are fixed, and the atoms in the right frames are tensioned horizontally. The tensile velocity  $v$  takes 0.06, 0.09 or 0.12 nm/ps, i.e. the displacement of 0.06, 0.09 or 0.12 nm is applied per 1000 time-steps. Among the empirical model potentials that have been developed for carbon molecular-systems, the Tersoff potential [12,13], based on the concept of bond order, is recognized to be the most successful one. Recently the second-generation Brenner potential [14] improves analytic function for the intra-molecular interaction which results in a significantly

better description of bond length, energy and force constant. However, in many works about carbon system [15], the Tersoff potential is still used. In this paper we use the Tersoff potential to describe the interaction of the bonded carbon atoms. For two neighbouring carbon atoms  $i$  and  $j$ , the Tersoff form of the energy  $\Phi$  is taken to be [12,13]

$$\Phi = \sum_i \sum_{j>i} f_c(r_{ij}) [E_r(r_{ij}) - b_{ij} E_a(r_{ij})] \quad (1)$$

with

$$E_r(r_{ij}) = A \exp(-\lambda r_{ij}) \quad (2)$$

$$E_a(r_{ij}) = B \exp(-\mu r_{ij})$$

$$f_c(r_{ij}) = \begin{cases} 1 & r_{ij} < R \\ \frac{1}{2} \left[ 1 + \cos \left( \pi \frac{r_{ij}-R}{S-R} \right) \right] & R < r_{ij} < S \\ 0 & S < r_{ij} \end{cases}$$

$b_{ij}$  is the many-body order parameter describing how the bond-formation energy is affected by the local atomic arrangement due to the presence of other neighbouring atoms (the  $k$ -atoms). It is a many-body function of the positions of the atoms  $i$ ,  $j$  and  $k$ . It has the form of

$$b_{ij} = \chi \left( 1 + \beta^n \xi_{ij}^n \right)^{-\frac{m}{2n}} \quad (3)$$

with

$$\xi_{ij} = \sum_{k \neq i,j} f_c(r_{ik}) \omega g(\theta_{ijk}) \quad (4)$$

$$g(\theta_{ijk}) = 1 + \frac{c^2}{d^2} - \frac{c^2}{d^2 + (h + \cos \theta_{ijk})^2}$$

where,  $r_{ij}$  is the distance of the  $i$ th and  $j$ th atom,  $\theta_{ijk}$  is the angle between  $r_{ij}$  and  $r_{jk}$ ,  $f_c(r_{ij})$  is a truncation function.  $A, B, \lambda, \mu, \chi, \beta, n, m, \omega, c, d, h, R$  and  $S$  are some correlative constants with the  $i$ - $j$ - $k$  atomic system, and their values take the corresponding ones in Ref. [12] and [13].

Considering the fact that the interaction of the unbonded carbon atoms is comparatively small the unbonded interaction is ignored in the simulations. The time step  $\Delta t$  takes 0.001 ps, and the temperature 300 K. The ensemble takes the NTV one, and the velocity the Verlet's expression [16].

### 3. Results and discussion

#### 3.1 The fracture modes

Figure 2 (a)–(d) presents the fracture modes of the presented C<sub>60</sub> layers/chain with  $v = 0.06$  and  $0.12$  nm/ps. In figure 2 the arrows are used to mark the start positions and propagation paths of the cracks, and the numbers of “1” and “2” indicate the cracking sequence of the cracks. The fracture modes of the C<sub>60</sub> layers/chain with  $v = 0.09$  nm/ps is very similar to the cases of  $v = 0.06$  nm/ps, and are not given here.

According to figure 2, it can be found that:

- (1) The C<sub>60</sub> layers (or C<sub>60</sub> chain) crack between two row (or two) C<sub>60</sub> fullerenes, and the cracks are perpendicular to the tensile direction. After fracture, all the C<sub>60</sub> fullerenes in the C<sub>60</sub> layers/chain have little change in structure.
- (2) The C<sub>60</sub> fullerenes in the C<sub>60</sub> polymers are elongated in the tensile direction and are shortened perpendicular to the tensile direction during the tension, namely the C<sub>60</sub> fullerenes become ellipsoids during the tension.
- (3) The C<sub>60</sub> layers (or C<sub>60</sub> chain) with different tensile velocity have obviously different fracture modes. Namely, the no-defect C<sub>60</sub> layer with  $v = 0.06$  and  $0.12$  nm/ps cracks between the two row C<sub>60</sub> fullerenes most close to the loading end, but, for the case of  $v = 0.06$  nm/ps, another incidental crack still appears between the second and third row fullerenes, see figure 2 (a); the single-edge defect C<sub>60</sub> layer with  $v = 0.06$  and  $0.12$  nm/ps does not crack from the defect, instead between the second and third row fullerenes, but, for the case of  $v = 0.06$  nm/ps, the start position of crack is close to the center of the C<sub>60</sub> layer, and for  $v = 0.12$  nm/ps the start position lies at the side with no defect, see figure 2 (b); the central defect C<sub>60</sub> layer with  $v = 0.06$  and  $0.12$  nm/ps cracks from the central defect, but the start position of crack is still slightly

different, see figure 2 (c); the C<sub>60</sub> chain with  $v = 0.06$  nm/ps fractures between the second and third C<sub>60</sub> fullerene close to the loading end, but, for the case of  $v = 0.12$  nm/ps, the C<sub>60</sub> chain fractures between the first and second C<sub>60</sub> fullerene, see figure 2 (d).

- (4) The single-edge defect C<sub>60</sub> layer does not crack, but the central defect C<sub>60</sub> layer from its defect, which implies that the cracking of the C<sub>60</sub> layers is more sensitive to the central defect. So it is predictable that, of the presented C<sub>60</sub> layers, the central defect one will have the worst mechanical properties.

#### 3.2 The tensile curves

Figure 3 shows the stress-strain curves ( $\sigma$ – $\varepsilon$  curves) of the C<sub>60</sub> layers/chain with  $v = 0.06, 0.09$  and  $0.12$  nm/ps. Here the tensile-stress  $\sigma$  is defined as  $\sigma = F/S$ , in which  $F$  is the external loading, and  $S$  is the tensile area. For the C<sub>60</sub> layers  $S = D \times L$ , and for the C<sub>60</sub> chain  $S = D^2$ . The tensile strain  $\varepsilon$  is defined as  $\varepsilon = \Delta L/L$ , in which  $\Delta L$  is the tensile displacement. In figure 3 the arrows  $\leftarrow$  mark the moment of the C<sub>60</sub> layers/chain cracking.

From figure 3, it is shown that:

- (1) With the tensile strain  $\varepsilon$  increasing, the stress  $\sigma$  for the C<sub>60</sub> layers/chain increases zigzaggedly, reaches the maximum  $\sigma_c$  at the positions marked by “ $\leftarrow$ ”, and then decreases quickly until the C<sub>60</sub> layers/chain fail, where the maximal stress  $\sigma_c$  is called as fracture stress and the corresponding strain  $\varepsilon_c$  are defined as the failure strain.
- (2) Within the range of  $\varepsilon < \varepsilon_c$ , for the same strain  $\varepsilon$ , all the three C<sub>60</sub> layers have larger stress than the 7C<sub>60</sub> chain, and the no-defect C<sub>60</sub> layer has slightly larger stress than two other C<sub>60</sub> layers. The phenomenon can be explained as followings: Firstly, in the C<sub>60</sub> layers there are lots of C–C bonds that are perpendicular to the tensile direction and between the C<sub>60</sub> fullerenes, during the tension the C–C bonds are tensioned and hinder the shrinkage of C<sub>60</sub> fullerenes perpendicular to the tensile direction, so, for the same tensile strain  $\varepsilon$ , the three C<sub>60</sub> layers have larger tensile-stress  $\sigma$  than the 7C<sub>60</sub> chain; secondly, the single-edge and central defects reduce the load support capability of the C<sub>60</sub> layer, so, for the same tensile strain  $\varepsilon$ , the no-defect C<sub>60</sub> layer has larger stress than the single-edge and central defect C<sub>60</sub> layers.
- (3) The fracture stress  $\sigma_c$  and the fracture strain  $\varepsilon_c$  are often used to characterize the fracture strength and the deformation capability of materials respectively. Generally, the larger the  $\sigma_c$  and  $\varepsilon_c$  are, the higher the fracture strength and the deformation capability of materials are. According to figure 3, apparently the fracture strength of the C<sub>60</sub> polymers has the order of “no-defect C<sub>60</sub> layer > single-edge defect C<sub>60</sub> layer > central defect C<sub>60</sub> layer > 7C<sub>60</sub> chain”, and the fracture strain, namely the deformation

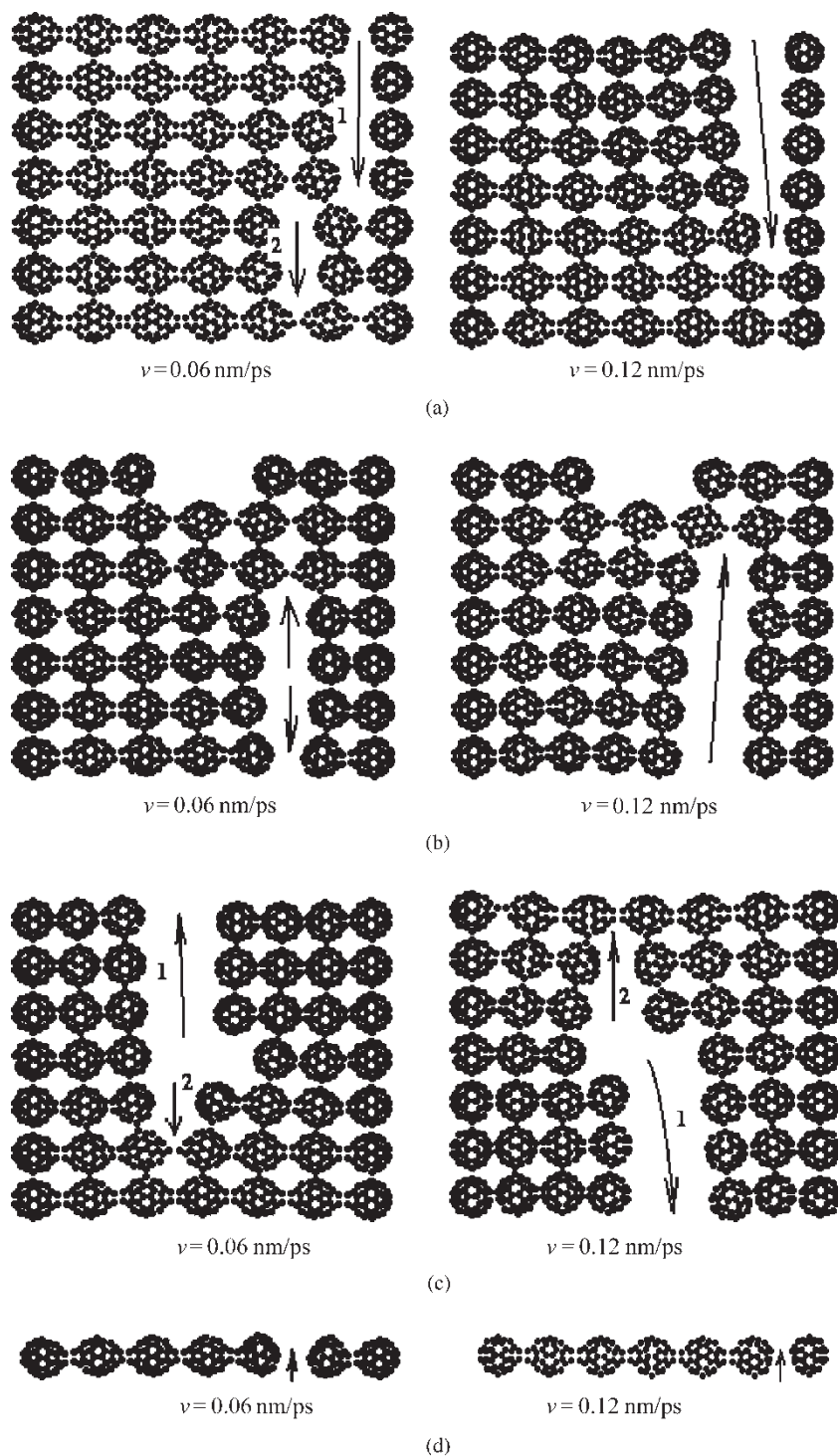


Figure 2. Tensile fracture of the  $C_{60}$  layers/chain. (a) no-defect  $C_{60}$  layer; (b) single-edge defect  $C_{60}$  layer; (c) central defect  $C_{60}$  layer; and (d)  $7C_{60}$  chain.

capability, has the order of “no-defect  $C_{60}$  layer > single-edge defect  $C_{60}$  layer >  $7C_{60}$  chain > central defect  $C_{60}$  layer”.

### 3.3 The effects of tensile velocity on tensile properties

Figure 4 presents the  $\sigma$ – $\varepsilon$  curves of the  $C_{60}$  layers/chain with different tensile velocity. According to figure 4,

it is found that the  $\sigma$ – $\varepsilon$  curves the  $C_{60}$  layers/chain under different tensile velocity are distinctly different. Firstly, the  $C_{60}$  layer/chain with low tensile-velocity has much smaller fracture strength  $\sigma_c$  but much higher fracture strain  $\varepsilon_c$  than that with high velocity. Secondly, for the same strain, the stress of the  $C_{60}$  layer/chain with high tensile-velocity is obviously larger than that with low velocity.



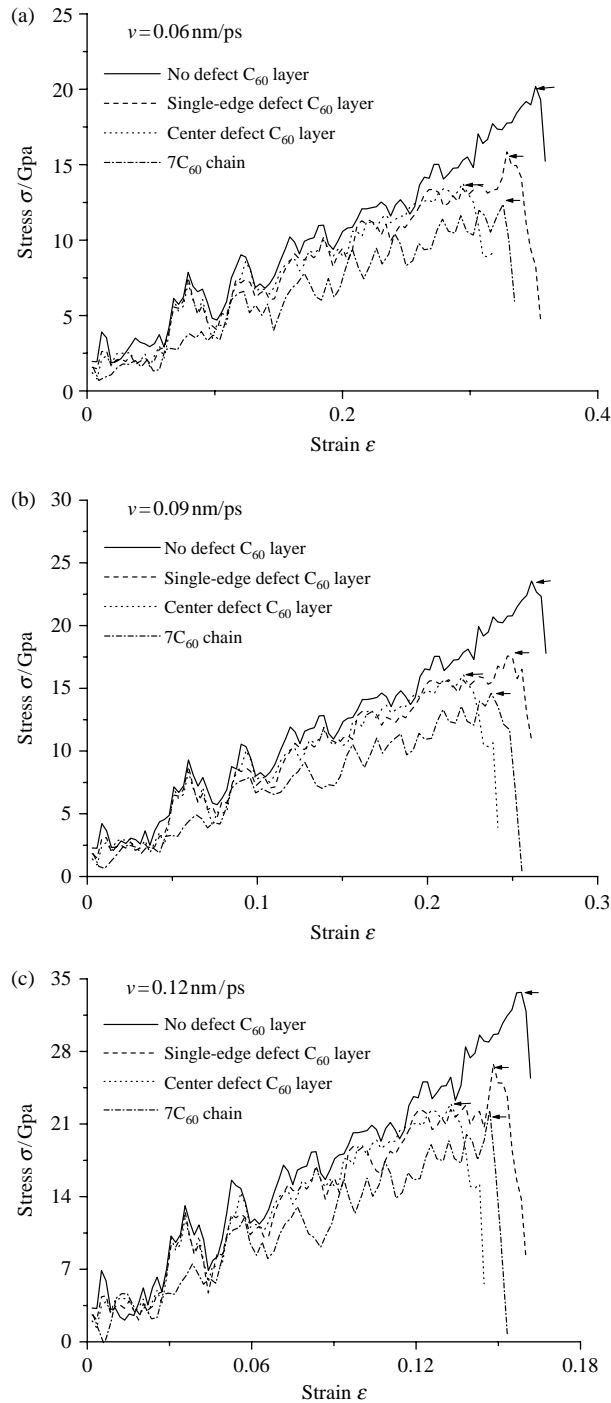


Figure 3. The  $\sigma$ - $\epsilon$  curves of the C<sub>60</sub> layers/chain with (a)  $v = 0.06$ ; (b)  $v = 0.09$ ; and (c)  $v = 0.12$  nm/ps.

Table 1 lists the fracture strength  $\sigma_c$ , fracture strain  $\epsilon_c$  and elastic module  $E$  for all the C<sub>60</sub> layers/chain with  $v = 0.06, 0.09$  and  $0.12$  nm/ps. Here the elastic module  $E$  is estimated according to the following method: linearly fitting all the  $\sigma$ - $\epsilon$  curves for  $\sigma < \sigma_c$  in the famous data-processing software of Origin 6, and approximatively regarding the slope of the fitted lines as the corresponding  $E$ .

Table 1 indicates that: (1) the elastic module  $E$  of all the C<sub>60</sub> layers/chain with high tensile velocity is larger than

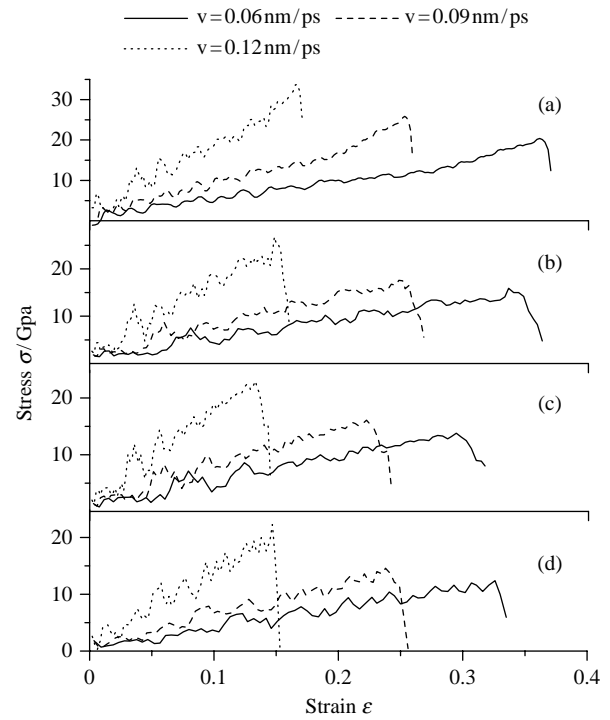


Figure 4. The  $\sigma$ - $\epsilon$  curves of (a) the no-defect C<sub>60</sub> layer; (b) the single edge-defect C<sub>60</sub> layer; (c) the central defect C<sub>60</sub> layer; and (d) the 7C<sub>60</sub> chain under different tensile velocity.

the ones with low velocity; (2) for the same tensile velocity the C<sub>60</sub> layers have higher  $E$  than the C<sub>60</sub> chain and the no-defect C<sub>60</sub> layer has the higher  $E$  than the other C<sub>60</sub> layers; (3) all the C<sub>60</sub> layers/chain with  $v = 0.06, 0.09$  or  $0.12$  nm/ps have the fracture strain  $\epsilon_c$  of  $13.4 \sim 35.9\%$ , the fracture strength  $\sigma_c$  of  $12.3 \sim 34.0$  GPa and the elastic module  $E$  of  $37.8 \sim 209.8$  GPa. The fracture strain  $\epsilon_c$  is comparable to that of steel,  $25 \sim 55\%$ , the elastic module  $E$  is lower than that of steel,  $200$  GPa; but the fracture strength  $\sigma_c$  is much higher than that of steel,  $0.25 \sim 0.33$  GPa. Here all the  $\epsilon_c$ ,  $E$  and  $\sigma_c$  data for steel come from reference [17]. This implies that the C<sub>60</sub> layers/chain in the present paper are a kind super-high-strength material.

Table 1. Fracture strength  $\sigma_c$ , fracture strain  $\epsilon_c$  and elastic module  $E$  for C<sub>60</sub> layers/chain.

Tensile velocity $v$ /nm/ps	C <sub>60</sub> polymer	$\sigma_c$ /GPa	$\epsilon_c$ /%	$E$ /GPa
0.06	No defect layers	20.3	35.9	56.5
	Single-edge defect layer	15.7	33.3	47.1
	Center defect layer	13.6	29.2	46.6
	7C <sub>60</sub> chain	12.3	32.5	37.8
0.09	No defect layers	25.2	26.1	96.6
	Single-edge defect layer	17.9	24.8	72.2
	Center defect layer	16.6	22.5	73.8
	7C <sub>60</sub> chain	14.9	23.8	62.6
0.12	No defect layers	34.0	16.1	209.8
	Single-edge defect layer	26.7	14.8	180.4
	Center defect layer	24.9	13.4	185.8
	7C <sub>60</sub> chain	21.6	14.7	146.9

#### 4. Conclusions

The Tersoff potential based MD simulations were performed to analyze the tensile fracture of three polymeric C<sub>60</sub> fullerene layers, with no defect, single-edge defect or central defect, and one polymeric 7C<sub>60</sub> fullerene chain. The effects of different type defect and tensile velocity on the tensile mechanical properties of the C<sub>60</sub> layers/chain were compared and discussed. The results are concluded as follows:

- (1) The C<sub>60</sub> layers, with different type defect and tensile velocity, have different fracture modes.
- (2) The fracture strength for the presented C<sub>60</sub> layers/chain conforms to the order of “no-defect C<sub>60</sub> layer > single-edge defect C<sub>60</sub> layer > central defect C<sub>60</sub> layer > 7C<sub>60</sub> chain”, and the deformation capability the order of “no-defect C<sub>60</sub> layer > single-edge defect C<sub>60</sub> layer > 7C<sub>60</sub> chain > central defect C<sub>60</sub> layer”.
- (3) The C<sub>60</sub> layers/chain with high tensile-velocity have higher fracture strength, higher elastic module but lower deformation capability than those with low velocity. For the same tensile velocity the C<sub>60</sub> layers have higher *E* than the C<sub>60</sub> chain, and the no-defect C<sub>60</sub> layer has the higher *E* than the two other C<sub>60</sub> layers.
- (4) The C<sub>60</sub> layers/chain have much higher tensile strength but lower elastic module than steel.

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